Plastics Manager



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General

Located under various

Functionality

- Adding new plastic materials to the KS database
- Automatic generation of the corresponding DAT files

If fatigue data from gear testing is available

- Calculation of permissible tooth root/flank stresses for different lubrication regimes
- Statistical evaluation of cycles to failure
- 2 calculation cases possible
- Identical test gears for all tests (testing on the test bench)
- Different test gears used (Z12, Z14, Z15, Z16) mainly testing in actual applications

Possible to calculate wear factors and heat transfer coeffcients acc. to the VDI 2736





General

How to get permissible root/flank stresses from gear measurements?

		Sneed rom	Cuclos 10 ⁶	Poom T °C	Root T, °C	Flank T, °C	Flank T, °C	Failuro
	Torque, Mili	speed, thin	Cycles, 10	Room I, C	(failed gear)	(failed gear)	(counter gear)	Failure
1	4.50	500	15.345	20	20	20	20	root
2	4.50	500	15.821	20	20	20	20	root
3	3.39	500	0.874	150	150	150	150	root
4	3.39	500	0.834	150	150	150	150	root
5	5.20	500	8.347	20	20	20	20	root
6	5.20	500	8.167	20	20	20	20	root
7	4.18	500	3.849	100	100	100	100	root
8	4.18	500	3.725	100	100	100	100	root
9	4.18	500	0.254	150	150	150	150	root
10	4.18	500	0.284	150	150	150	15	root
11	5.08						0	root
12	5.08	R	esult	s troi	m aea	ar tesi	S o	root
13	5.08						2	root
14	5.08	500	1.922	100	100	100	100	root
15	5.08	500	0.092	150	150	150	150	Teet
16	5.08	500	0.074	150	150	150	150	root
17	6.21	500	3.806	20	20	20	20	root
18	6.21	500	3.486	20	20	20	20	root
19	6.21	500	0.405	100	100	100	100	root
20	6.21	500	0.425	100	100	100	100	root
21	6.78	500	1.722	20	20	20	20	root
22	6.78	500	1.951	20	20	20	20	root
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Number of load cycles

Use Plastics Manager

General – Tab basic data

eneral										
laterial name	Input			Densit	ty			P _{mat}	0.0000	kg/m³
omment	Input			Poisso	n's ratio			v	0.0000]
ata source	Input			Specific heat capacity				см 0.0000] J/(kg*K)	
laterial type	Thermoplastic PA		•	Specif	ic heat co	onductivity		λм	0.0000	W/(m*K)
ype of treatment	untreated		-	Coeff	cient of t	thermal exp	pansion	٥	0.0000	10 ⁻⁶ /°C
laterial group	Not on the list		•	Absor	ption of v	water		WVOL	0.0000	%
oefficient of frictio /ear coefficient	n	µ k _w	0.0000	0.0000		0.0000]] mm³/N	lm/10 ⁴	5	
/ear coefficient		kw	0.0000	0.0000		0.0000] mm ³ / N	lm/10 ⁶	5	
emperature depen	dent wear coefficient		No 🔻	No	Yes	•				
emperature depen	dent wear coefficient		θ [°C]	k _{w.p} [mm³/Nm/:	10°]			7		

General material properties

Tribological properties

Temperature dependent wear coefficients



General – Tab Test data and extrapolation

Dan	age probi	ability	5	0.0000 %	Stat	stical method Acc.	to VDI 2736-4	•		
Mer	ge temper	ature deviation	Δθ _{merge}	1.0000 °C	Test	gear file SABI	C_standard_geomet	ry.Z12		
Tore	ue merge	deviation	ΔΤ/Τ	1.0000 %	Faile	d gear 2		•		
Gro	in temper	ature deviation	Λθ	1.0000 °C						
fest	gear mea	surements								
	Status	T [Nm]	n [1/min]	N _L [10 ⁶]	θ _u [ºC]	θ_GUT _{root} [ºC]	θ_GUT _{flank} [°C]	Failure mode	θ_counter _{flank} [°C]	
7	active	4.1800	500.0000	3.8490	100.0000	100.0000	100.0000	Root	100.0000	
-	active	4.1800	500.0000	3.7250	100.0000	100.0000	100.0000	Root	100.0000	
8			500,0000	0.2540	150.0000	150.0000	150.0000	Root	150.0000	
8 9	active	4.1800	50010000							
8 9 10	active active	4.1800 4.1800	500.0000	0.2840	150.0000	150.0000	150.0000	Root	150.0000	
8 9 10 11	active active active	4.1800 4.1800 6.0000	500.0000	0.2840	150.0000 20.0000	150.0000 20.0000	150.0000 20.0000	Root Root	150.0000 20.0000	
8 9 10 11 12	active active active active	4.1800 4.1800 6.0000 6.0000	500.0000 500.0000 500.0000	0.2840 4.5440 4.3440	150.0000 20.0000 20.0000	150.0000 20.0000 20.0000	150.0000 20.0000 20.0000	Root Root Root	150.0000 20.0000 20.0000	



Extrapolation options

Basic data	Test data	Data extrapolation	DAT file							
Permissible tooth root stress										
Method 1		Extrapolate with average slope			Extend temperature range					
Extrapolate to cycles		10000.0000 105 🔫			Extend to temperature	θ⊧	0.0000	℃		
Method 2		Set cycles to infinity			Increase permissible stress by facto	1.0000				

To calculate safety factors with load spectrum in KISSsoft, S-N curves should be defined until 10³⁰ cycles. It is not possible to measure that long, so instead, extrapolation is used.

-- Permissible tooth root stress sigFlim [N/mm2], all lubrication regimes

-- Calculated with 10% damage probability

-- Calculated with root safety factor SF=1

-- Values with * measured, other interpolated/extrapolated

:TABLE FUNCTION FootSigFlim

INPUT X ZahnTempFuss TREAT LINEAR

INPUT Y Lastwechsel TREAT LOG

DATA			
	20	100	150
0.000e+000	33.3	30.5	25.0
7.709e+004	33.3	30.5	25.0*
2.492e+005	33.3	30.5	20.5*
3.839e+005	33.3	30.5*	19.0
7.865e+005	33.3	27.6	16.7
1.585e+006	33.3	25.0*	16.7
1.681e+006	33.3*	24.6	16.7
3.327e+006	30.5*	20.7	16.7
3.457e+006	30.3	20.5	16.7
4.053e+006	29.5*	20.5	16.7
7.503e+006	25.5*	20.5	16.7
1.411e+007	22.1	20.5	16.7
1.000e+099	22.1	20.5	16.7
END			



Damage probability



According to the VDI 2736-4, each test condition (torque, temperature) should be measured at least 3 times. The calculated average cycles to failure represent 50% damage probability.

Example: 143300, 100780 and 94020 cycles to failure (calculated standard deviation: 26715).

Damage probability	1%	5%	10%	20%	30%	40%	50%
Calculated cycles	50500 (-55%)	68700 (-40%)	78500 (-30%)	90250 (-20%)	98700 (-13%)	106000 (-6%)	112700

SOURCE: http://www.mathsisfun.com/definitions/standard-normal-distribution.html

Merge temperature and torque deviation

Dam	age prob	ability		50.0000 %			
Merg	ge temper	ature deviation		1.0000	°C		
Toro	lue merge	edeviation	1.0000		%		
Group temperature deviation $\Delta \theta_{group}$ 1.0000 °C							
Test gear measurements							
	Status	T [Nm]	n [1/mi	n]	N _L [10 ⁶]	θυ
7	active	4.1800	5	00.0000		3.8490	
8	active	4.1800	5	00.0000		3.7250	
9	active	4.1800	5	00.0000		0.2540	
10	active	4.1800	5	00.0000		0.2840	
11	active	6.0000	5	00.0000		4.5440	
12	active	6.0000	5	00.0000		4.3440	
		E 0000				4 6640	

	Torque	Speed	Root θ	NL
1	1.00 Nm	750 rpm	100 ºC	1.01·10 ⁶
2	1.05 Nm	750 rpm	120 °C	1.13·10 ⁶
3	1.00 Nm	750 rpm	105 ⁰C	0.82·10 ⁶
4	1.00 Nm	750 rpm	98 °C	1.05·10 ⁶
5	0.98 Nm	750 rpm	102 ⁰C	0.88 [.] 10 ⁶

According to the VDI 2736-4, each test condition (torque, temperature) should be measured at least 3 times.

 $\Delta \theta_{merge} = 8^{\circ}C$ and $\Delta T/_T = 5\%$ Tests 1, 3, 4, 5 merged together $\Delta \theta_{merge} = 3^{\circ}C$ and $\Delta T/_T = 2\%$ Tests 1, 4, 5 merged together

Torque: 0.98 Nm Root temperature: 98 °C NL: 0.80·10⁶ (10% failure) Torque: 0.98 Nm Root temperature: 98 °C NL: 0.87·10⁶ (10% failure)

Points, that are merged together, form only 1 point on the S-N curve.



Group temperature deviation

Dam	age prob	ability		5	0.0000	%		
Merg	ge temper	rature deviation <i>l</i>	∆0 _{merge}	1.0000 °C				
Toro	lue merge	deviation	∆т/т		1.0000	%		
Group temperature deviation ∆θ _{group} 1.0000 ℃								
Test gear measurements								
	Status	T [Nm]	n [1/mi	n]	N _L [10 ⁶]	θυ	
7	active	4.1800	5	00.0000		3.8490		
8	active	4.1800	5	00.0000		3.7250		
9	active	4.1800	5	00.0000		0.2540		
10	active	4.1800	5	00.0000		0.2840		
11	active	6.0000	5	00.0000		4.5440		
12	active	6.0000	5	00.0000		4.3440		
		E 0000	-					

	Root stress	Root T	NL
1	55 MPa	41 ⁰C	1.00 [.] 10 ⁶
2	45 MPa	42 °C	2.10 [.] 10 ⁶
3	35 MPa	44 °C	3.80·10 ⁶
4	28 MPa	50 °C	4.00 [.] 10 ⁶
5	15 MPa	80 °C	5.00·10 ⁶

According to the VDI 2736-4, S-N curve at 1 temperature should be measured at 4 different loads (root stresses)

 $\Delta \theta_{group} = 10^{\circ}C$ Tests 1, 2, 3, 4 grouped together

root T = 41 $^{\circ}$ C

$$\Delta \theta_{group} = 4^{\circ}C$$

Tests 1, 2, 3 grouped together

root T = 41 $^{\circ}$ C

SigFlim	values	noted wit	th * were measu
:TABLE FUN	CTION F	ootSigFli	n
INPU	T X Zah	nTempFuss	TREAT LINEAR
INPU	T Y Las	twechsel	TREAT LOG
DATA			
	20	80	
0.000E+00	41.5	27.7	
1.000E+05	41.5*	27.7	
3.400E+05	34.6*	27.7	
3.600E+05	31.2*	27.7	
4.700E+05	30.6	27.7*	
6.000E+05	30.1	24.2*	
8.200E+05	29.4	20.8*	
1.770E+06	27.9	19.1*	
2.000E+06	27.7*	17.3*	
2.001E+06	0.0	0.0	
1.000E+99	0.0	0.0	
END			

-- Tooth root strength sigFlim [N/mm2] -



Summary of merge and group functions



KISS5

Calculating permissible stresses

The calculated permissible stresses are calculation method dependent.

		Safety factor lifetime calculation method			
		VDI 2736 (YF C)	VDI 2545 (YF C)	VDI 2545 (YF B)	
Permissible	VDI 2736 (YF C)	1.00 (254 h)	1.12 (529 h)	0.99 (247 h)	
stress calculation	VDI 2545 (YF C)	0.89 (125 h)	1.00 (254 h)	0.89 (122 h)	
method	VDI 2545 (YF B)	1.00 (260 h)	1.12 (570 h)	1.00 (254 h)	

Calculated safety factors and achieved lifetime with SF = 1 (steel/POM, 350 rpm, 20 °C, 10⁶ cycles).

The same calculation method should be used for permissible stress calculation and for the calculation of safety factors!



What and how to measure during testing

	Root failure	Flank failure	Wear factor	Heat transfer coefficients
Torque and speed	yes	yes	yes	yes
Cycles to failure	yes	yes	yes	no
Root temperature, failed	yes	no	no	yes
Root temperature, counter	no	no	no	yes
Flank temperature, failed	no	yes	yes	yes
Flank temperature, counter	no	no ^{*SP} /yes ^{*PP}	no	yes
Local linear wear or mass	no	no	yes	no

*SP – steel/plastic combination, *PP – for plastic/plastic combination



SOURCE: Kalin M. et. al: Temperature dependent tribological behaviour of polymer (POM) gears, 2017. Industriekreis final report, Lehrstuhl für Kunststofftechnik Universität Erlangen-Nürnberg, 2010. 11 Plastics Manager - CONFIDENTIAL



Additional options

It is also possible to calculate and combine permissible stresses from **different** test geometries – testing in actual applications. However, the material of failed gear must be the same!





Thank you!



