

KISSsoft evaluation

File

Name : PlanetarySet 1 (ISO6336)
 Description: KISSsoft example
 Changed by: kspl on: 07.03.2016 at: 10:51:33

Important hint: At least one warning has occurred during the calculation:

1-> The calculation of micropitting specified in ISO15144 is not designed for use with internal toothing because it has not yet been subject to sufficient investigation.
 The results can only be used for information purposes.

CALCULATION OF A SPUR PLANETARY GEAR

Drawing or article number:

Gear 1: 0.000.0
 Gear 2: 0.000.0
 Gear 3: 0.000.0

Calculation method ISO 6336:2006 Method B

		----- Sun -----	----- Planets
----- Internal gear ---			
Number of planets (1)	[p]	(1)	3
Power (W) .000	[P]		700
Speed (1/min) 0.0	[n]	1200.0	
Speed difference for planet bearing calculation (1/min)	[n2]		760.5
Speed planet carrier (1/min)	[nSteg]		266.7
Torque (Nm) .000	[T]	5.570	0
Torque Pl.-Carrier (Nm) .067	[TSteg]	19.496	25

Fatigue strength. tooth root stress (N/mm ²) 290.00	[sigFlim]	430.00	430.00
Fatigue strength for Hertzian pressure (N/mm ²) 700.00	[sigHlim]	1500.00	1500.00
Tensile strength (N/mm ²) 1200.00	[Rm]	1200.00	1200.00
Yield point (N/mm ²) 1000.00	[sigs]	850.00	850.00
Young's modulus (N/mm ²) 206000	[E]	206000	206000
Poisson's ratio 0.300	[ny]	0.300	0.300
Roughness average value DS, flank (µm) 1.05	[RAH]	0.60	0.60
Roughness average value DS, root (µm) 3.00	[RAF]	3.00	3.00
Mean roughness height, Rz, flank (µm) 8.00	[RZH]	4.80	4.80
Mean roughness height, Rz, root (µm) 20.00	[RZF]	20.00	20.00

Gear reference profile	1 :		
Reference profile	1.25 / 0.38 / 1.0 ISO 53.2:1997 Profil A		
Dedendum coefficient	[hfP*]		1.250
Root radius factor 0.472)	[rhofP*]		0.380 (rhofPmax*=
Addendum coefficient	[haP*]		1.000
Tip radius factor	[rhoaP*]		0.000
Protuberance height factor	[hprP*]		0.000
Protuberance angle	[alfprP]		0.000
Tip form height coefficient	[hFaP*]		0.000
Ramp angle	[alfKP]		0.000

not topping

Gear reference profile	2 :		
Reference profile	1.25 / 0.38 / 1.0 ISO 53.2:1997 Profil A		
Dedendum coefficient	[hfP*]		1.250
Root radius factor 0.472)	[rhofP*]		0.380 (rhofPmax*=
Addendum coefficient	[haP*]		1.000
Tip radius factor	[rhoaP*]		0.000
Protuberance height factor	[hprP*]		0.000
Protuberance angle	[alfprP]		0.000
Tip form height coefficient	[hFaP*]		0.000
Ramp angle	[alfKP]		0.000

not topping

Reference profile of tool from gear	3 :		
Pinion type cutter (Own input)	Eigene Eingabe		
Number of teeth	[z]		30
Profile shift coefficient	[x*]		0.100
Base diameter (mm)	[db0]		28.191
Addendum coefficient	[haP0*]		1.200
Tip diameter (mm)	[da0]		32.600
Tip form: Radius	[rhoaP0*]		0.200
Dedendum coefficient	[hfP0*]		1.250
Root diameter (mm)	[df0]		27.700
Root radius factor	[rhofP0*]		0.000
Tip form diameter (mm)	[dFa0]		32.395
Root form diameter (mm)	[dFf0]		28.412
		not topping	
Addendum coefficient Reference profile Gear	[haP*]		1.000
Summary of reference profile gears:			
Dedendum reference profile 1.148	[hfP*]	1.250	1.250
Tooth root radius Refer. profile 0.200	[rofP*]	0.380	0.380
Addendum Reference profile 1.000	[haP*]	1.000	1.000
Protuberance height factor 0.000	[hprP*]	0.000	0.000
Protuberance angle (°) 0.000	[alfprP]	0.000	0.000
Tip form height coefficient 0.000	[hFaP*]	0.000	0.000
Ramp angle (°) 0.000	[alfKP]	0.000	0.000
Type of profile modification:	none (only running-in)		
Tip relief (µm) 8.50	[Ca]	2.00	2.00
Lubrication type	oil bath lubrication		
Type of oil	Oil: Klüberoil GEM 1-220 N with details about		
wear coefficient kw			
Lubricant base	Mineral-oil base		
Kinem. viscosity oil at 40 °C (mm ² /s)	[nu40]		220.00
Kinem. viscosity oil at 100 °C (mm ² /s)	[nu100]		19.00
FZG test A/8.3/90 (ISO 14635-1:2006)	[FZGtestA]	14	
Specific density at 15 °C (kg/dm ³)	[roOil]		0.890
Oil temperature (°C)	[TS]		70.000

	----- Gear 1 -----	Gear 2 -----	Gear 3 ---
Overall transmission ratio	[itot]	4.500	
Gear ratio	[u]	1.227	
-2.852			
Transverse module (mm)	[mt]	1.000	
Pressure angle at pitch circle (°)	[alft]	20.000	
Working transverse pressure angle (°)	[alfwt]	24.498	
21.790			
	[alfwt.e/i]	24.550 /	24.445 21
.731 /	21.849		
Working pressure angle at normal section (°)	[alfwn]	24.498	
21.790			
Helix angle at operating pitch circle (°)	[betaw]	0.000	
0.000			
Base helix angle (°)	[betab]	0.000	
Reference centre distance (mm)	[ad]	24.500	
-25.000			
Sum of profile shift coefficients	[Summexi]	0.8890	
-0.3131			
Profile shift coefficient	[x]	0.4575	0.4315
-0.7446			
Tooth thickness (Arc) (module) (module)	[sn*]	1.9038	1.8849
1.0288			
Tip alteration (mm)	[k*mn]	-0.089	-0.089
0.000			
Reference diameter (mm)	[d]	22.000	27.000
-77.000			
Base diameter (mm)	[db]	20.673	25.372
-72.356			
Tip diameter (mm)	[da]	24.737	29.685
-76.489			
(mm)	[da.e/i]	24.737 /	24.727 29.685 / 29
.675 -76.489 /	-76.499		
Tip diameter allowances (mm)	[Ada.e/i]	0.000 /	-0.010 0.000 / -0
.010	0.000 /	-0.010	
Tip form diameter (mm)	[dFa]	24.737	29.685
-76.489			
(mm)	[dFa.e/i]	24.737 /	24.727 29.685 / 29
.675 -76.489 /	-76.499		
Active tip diameter (mm)	[dNa.e/i]	24.737 /	24.727 29.685 / 29
.675	-76.489 /	-76.499	
Operating pitch diameter (mm)	[dw]	22.718	27.882 / 27
.324	-77.924		
(mm)	[dw.e]	22.728	27.893 / 27
.313 -77.892			

	(mm)	[dw.i]	22.709	27.870 /	27
.335	-77.956				
Root diameter (mm)		[df]	20.415	25.363	
-80.785					
Generating Profile shift coefficient		[xE.e/i]	0.3833 /	0.3421	0.3573 /
.3161		-0.8407 /	-0.8957		0
Manufactured root diameter with xE (mm)		[df.e]	20.267	25.215	
-80.948					
	(mm)	[df.i]	20.184	25.132	
-81.040					
Theoretical tip clearance (mm)		[c]	0.250	0.250/	0.250
0.263					
Tip clearance upper allowance (mm)		[c.e]	0.381	0.381/	0.393
0.394					
Tip clearance lower allowance (mm)		[c.i]	0.314	0.314/	0.321
0.327					
Active root diameter (mm)		[dNf]	21.411	26.428/	26.076
-80.029					
	(mm)	[dNf.e]	21.429	26.447/	26.096
-79.997					
	(mm)	[dNf.i]	21.398	26.414/	26.063
-80.053					
Root form diameter (mm)		[dFf]	21.126	26.051	
-80.476					
	(mm)	[dFf.e/i]	21.041 /	20.998	25.956 /
.906	-80.654 /	-80.753			25
Reserve (dNf-dFf)/2 (mm)		[cF.e/i]	0.216 /	0.178	0.095 /
.053		0.378 /	0.300		0
Addendum (mm)		[ha = mn * (haP*+x)]		1.369	1
.343		0.255			
	(mm)	[ha.e/i]	1.369 /	1.364	1.343 /
1.338	0.255 /	0.250			
Dedendum (mm)		[hf = mn * (hfP*-x)]		0.793	0
.818		1.893			
	(mm)	[hf.e/i]	0.867 /	0.908	0.893 /
0.934	1.974 /	2.020			
Roll angle at dFa (°)		[xsi_dFa.e/i]	37.649 /	37.599	34.801 /
34.757		19.640 /	19.664		
Roll angle to dNf (°)		[xsi_dNf.e/i]	15.634 /	15.300	16.860 /
16.590					
		[xsi_dNf.e/i]		13.790 /	13.465
27.016 /		27.121			
Roll angle at dFf (°)		[xsi_dFf.e/i]	10.860 /	10.192	12.368 /
11.824		28.215 /	28.393		
Tooth height (mm)		[H]	2.161	2.161	
2.148					
Virtual gear	no. of teeth	[zn]	22.000	27.000	

-77.000						
Normal-tooth thickness at tip circle (mm)	[san]	0.636		0.688		
0.842						
	(mm)	[san.e/i]	0.581 /	0.541	0.634 /	0.595
0.776 /	0.733					
Normal space width at root circle (mm)	[efn]	0.000		0.000		
0.540						
	(mm)	[efn.e/i]	0.000 /	0.000	0.000 /	0.000
0.533 /	0.529					
Max. sliding velocity at tip (m/s)	[vga]	0.369		0.341/ 0.136		
0.107						
Specific sliding at the tip	[zetaa]	0.556		0.556/ 0.222		
0.308						
Specific sliding at the root	[zetaf]	-1.254		-1.254/ -0.445		
-0.285						
Sliding factor on tip	[Kga]	0.333		0.307/ 0.125		
0.098						
Sliding factor on root	[Kgf]	-0.307		-0.333/ -0.098		
-0.125						
Pitch on reference circle (mm)	[pt]			3.142		
Base pitch (mm)	[pbt]			2.952		
Transverse pitch on contact-path (mm)	[pet]			2.952		
Length of path of contact (mm)	[ga]			4.007		4
.696						
	(mm)			[ga.e/i]		4
.032 /	3.963			4.724 /		4
.642						
Length T1-A (mm)	[T1A]	2.786		7.705/ 3.010		
-12.401						
Length T1-B (mm)	[T1B]	3.840		6.651/ 4.753		
-14.145						
Length T1-C (mm)	[T1C]	4.710		5.781/ 5.071		
-14.463						
Length T1-D (mm)	[T1D]	5.738		4.753/ 5.962		
-15.353						
Length T1-E (mm)	[T1E]	6.792		3.699/ 7.705		
-17.097						
Diameter of single contact point B (mm)	[d-B]	22.054		28.647/	27.094	
-77.690						
(mm)	[d-B.e]	22.054		28.623/	27.094	
-77.710						
(mm)	[d-B.i]	22.047		28.679/	27.087	
-77.662						
Diameter of single contact point D (mm)	[d-D]	23.645		27.094/	28.034	
-78.602						
(mm)	[d-D.e]	23.620		27.094/	28.010	
-78.602						

(mm) -78.614	[d-D.i]	23.679	27.087/	28.071
Transverse contact ratio .591	[eps_a]	1.357		1
Transverse contact ratio with allowances .572	[eps_a.e/i]	1.366 /	1.342	1.600 / 1
Overlap ratio .000	[eps_b]	0.000		0
Total contact ratio .591	[eps_g]	1.357		1
Total contact ratio with allowances .572	[eps_g.e/i]	1.366 /	1.342	1.600 / 1

2. FACTORS OF GENERAL INFLUENCE

		----- Gear 1 -----	Gear 2 -----	Gear 3 ---
Nominal circum. force at pitch circle (N) 168.801	[Ft]		168.801	
Axial force (N) 0.0	[Fa]		0.0	0.0
Axial force (total) (N) 0.0	[Fatot=Fa* 3]		0.0	
Radial force (N) 61.438	[Fr]		61.438	
Normal force (N) 179.6	[Fnorm]		179.6	179.6
Nominal circumferential force per mm (N/mm) 33.76	[w]		33.76	
Only as information: Forces at operating pitch circle:				
Nominal circumferential force (N) 166.799	[Ftw]		163.463	
Axial force (N) 0.0	[Fa]		0.0	0.0/ 0.0
Axial force (total) (N) 0.0	[Fatot=Fa* 3]		0.0	
Radial force (N) 66.681	[Fr]		74.486	
Circumferential speed reference circle (m/s) (Planet)	[v]			1.08
Running-in value (µm) 1.063	[yp]		0.495	
Running-in value (µm) 0.987	[yf]		0.412	
Gear body coefficient	[CR, bs/b]		0.865 (0.250)	

0.865 (0.250)		
Correction coefficient	[CM]	0.800	
0.800			
Reference profile coefficient	[CBS]	0.975	
1.001			
Material coefficient	[E/Est]	1.000	
1.000			
Singular tooth stiffness (N/mm/μm)	[c']	9.844	
10.775			
Meshing stiffness (N/mm/μm)	[cgalf]	12.482	
15.547			
Meshing stiffness (N/mm/μm)	[cgbet]	10.609	
13.215			
Reduced mass (kg/mm)	[mRed]	0.0004	0
.0022			
Resonance speed (min-1)	[nE1]	72996	
29564			
Resonance ratio (-)	[N]	0.013	
0.026			
Running-in value (μm)	[ya]	0.495	
1.063			
Planet on rolling bearings. Planet pin fixed on both sides in carrier.			
lpa (mm) = 6.50 b (mm) = 5.00 dsh (mm) = 13.50			
Tooth trace deviation (active) (μm)	[Fby]	3.66	
3.34			
from deformation of shaft (μm)	[fsh*B1]	0.14	
0.00			
(fsh (μm) = 0.14/ 0.00, B1= 1.00/ 1.00, fHb5 (μm) = 4.50/ 4.80)			
Tooth trace		0	
0			
(0:without, 1:crowned, 2:Tip relief, 3:full modification)			
(4:Slightly crowned, 5:Helix angle modification, 6:Helix angle modification with crowning)			
from production tolerances (μm)	[fma*B2]	9.19	
9.19			
(B2=			
1.00/ 1.00)			
Tooth trace deviation, theoretical (μm)	[Fbx]	4.31	
4.80			
Running-in value y.b (μm)	[yb]	0.65	
1.46			
Dynamic factor	[KV=max(KV12,KV23)]		1.03
	[KV12,KV23]	1.01	
1.03			
Face load factor - flank	[KHb]	1.45	

1.51				
	- Tooth root	[KFb]		1.29
1.33				
	- Scuffing	[KBb]		1.45
1.51				
Transverse load factor - flank		[KHa]		1.00
1.16				
	- Tooth root	[KF _a]		1.00
1.16				
	- Scuffing	[KB _a]		1.00
1.16				
Helical load factor scuffing		[K _{bg}]		1.00
1.00				
Number of load cycles (in mio.)		[NL]	3360.0	912.6
960.0				

3. TOOTH ROOT STRENGTH

Calculation of Tooth form coefficients according method: B

Internal toothing: Calculation of roF and sFn according to

ISO 6336-3:2007-04-01

Internal toothing: Calculation of YF, YS

with pinion type cutter (z0=

30, x0= 0.100, rofP*= 0.200)

----- Gear 1 ----- Gear 2 ----- Gear 3 ---

Calculated with manufacturing profile shift	[xE.e]	0.38	0.36
-0.84			
Tooth form factor	[YF]	1.55	1.56/ 1.19
1.04			
Stress correction factor	[YS]	2.01	2.00/ 2.23
2.41			
Bending lever arm (mm)	[hF]	1.27	1.30/ 0.97
1.33			
Working angle (°)	[alfFen]	26.13	25.30/ 22.19
22.26			
Tooth thickness at root (mm)	[sFn]	2.17	2.19/ 2.19
2.74			
Tooth root radius (mm)	[roF]	0.45	0.45/ 0.45
0.43			

(hF* = 1.270/ 1.297/ 0.966/ 1.326 sFn* = 2.168/ 2.191/ 2.191/ 2.741)

(roF* = 0.450/ 0.451/ 0.451/ 0.434 dsFn = 20.601/ 25.563/ 25.563/ -80.882 alfsFn = 30.0/ 30.0/ 30.0/ 60.0)

Helix angle factor	[Ybet]	1.00	1.00
Deep tooth factor	[YDT]	1.00	1.00

Gear rim factor 1.00	[YB]	1.00	1.00
Effective facewidth (mm) 5.00	[beff]	5.00	5.00/ 5.00
Nominal stress at tooth root (N/mm ²) 84.86	[sigF0]	104.87	105.57/ 89.48
Tooth root stress (N/mm ²) 169.03	[sigF]	174.48	175.64/ 178.24
Permissible bending stress at root of Test-gear Notch sensitivity factor 1.004	[YdrelT]	0.999	0.999/ 0.999
Surface factor 0.957	[YRrelT]	0.957	0.957
size factor (Tooth root) 1.000	[YX]	1.000	1.000
Finite life factor 0.891	[YNT]	0.869	0.892
Alternating bending factor (mean stress influence coefficient) 1.000	[YM]	1.000	0.700
Stress correction factor Yst*sigFlim (N/mm ²) 580.00	[Yst] [sigFE]	860.00	2.00 860.00
Permissible tooth root stress (N/mm ²) 413.65	[sigFP=sigFG/SFmin]	595.17	427.73/ 427.73
Limit strength tooth root (N/mm ²) 496.38	[sigFG]	714.21	513.27/ 513.27
Required safety 1.20	[SFmin]	1.20	1.20
Safety for Tooth root stress 2.94	[SF=sigFG/sigF]	4.09	2.92/ 2.88
Transmittable power (kW) 1.71	[kWRating]	2.39	1.70/ 1.68

4. SAFETY AGAINST PITTING (TOOTH FLANK)

		----- Gear 1 -----	Gear 2 -----	Gear 3 ---
Zone factor	[ZH]		2.23	2.38
Elasticity coefficient ($\sqrt{N/mm}$)	[ZE]		189.81	189.81
Contact ratio factor	[Zeps]		0.939	0.896
Helix angle factor	[Zbet]		1.000	1.000
Effective facewidth (mm)	[beff]		5.00	5.00
Nominal flank pressure (N/mm ²)	[sigH0]		662.83	364.84
Surface pressure at operating pitch circle (N/mm ²)	[sigHw]		904.93	548.49

Single tooth contact factor 1.00	[ZB,ZD]	1.03	1.00/ 1.04
Flank pressure (N/mm ²) 548.49	[sigHB, sigHD]	934.36	904.93/ 572.91
Lubrication coefficient at NL 1.038	[ZL]	1.020	1.020/ 1.038
Speed coefficient at NL 0.904	[ZV]	0.955	0.955/ 0.904
Roughness coefficient at NL 0.882	[ZR]	0.929	0.929/ 0.882
Work hardening factor at NL 1.003	[ZW]	1.000	1.000/ 1.000
Finite life factor 0.913	[ZNT]	0.879	0.915
Small no. of pittings permissible:	no		
Size factor (flank) 1.000	[ZX]	1.000	1.000
Permissible surface pressure (N/mm ²) 589.65	[sigHP=sigHG/SHmin]	1326.15	1380.25/ 1261.33
Limit strength pitting (N/mm ²) 530.68	[sigHG]	1193.54	1242.22/ 1135.20
Required safety 0.90	[SHmin]	0.90	0.90
Safety for surface pressure at operating pitch circle 0.97	[SHw]	1.32	1.37/ 2.07
Safety for stress at single tooth contact 0.97	[SHBD=sigHG/sigHBD]	1.28	1.37/ 1.98
(Safety regarding transmittable torque) 0.94	[(SHBD)^2]	1.63	1.88/ 3.93
Transmittable power (kW) 0.81	[kWRating]	1.41	1.63/ 3.39

4b. MICROPITTING ACCORDING TO ISO/TR 15144-1:2014

Pairing Gear 1-2:

Calculation of permissible specific film thickness

Lubricant load according to FVA Info sheet 54/7 10 (Oil: Klüberoil GEM 1-220 N with details about wear coefficient kw)

Reference data FZG-C Test:

Torque (Nm)	[T1Ref]	265.1
Line load at contact point A (N/mm)	[FbbRef,A]	236.3
Oil temperature (°C)	[theOilRef]	90.0
Tooth mass temperature (°C)	[theMRef]	127.7

Contact temperature (°C)	[theBRef,A]	251.7
Lubrication gap thickness (µm)	[hRef,A]	0.051
Specific film thickness in test (µm)	[lamGFT]	0.102
Material coefficient	[WW]	1.00
Permissible specific film thickness (µm)	[lamGFP]	0.143

Interim results in accordance with ISO/TR 15144:2014

Coefficient of friction	[mym]	0.111
Lubricant factor	[XL]	1.000
Roughness factor	[XR]	1.525
Tooth mass temperature (°C)	[theM]	72.7
Tip relief factor	[XCa (A)]	1.272
Loss factor	[HV]	0.146
Equivalent Young's modulus (N/mm ²)	[Er]	226374
Compressed viscosity index (m ² /N)	[alf38]	0.02162
Dynamic viscosity (Ns/m ²)	[etatM]	39.6
Roughness average value (µm)	[Ra]	0.6

Calculation of speeds, load distribution and flank curvature according to method B following ISO/TR 15144-1:2014

Ca taken as optimal in the calculation (0=no, 1=yes)	0	0	
Calculation at point (0:A, 1:AB, 2:B, 3:C, 4:D, 5:DE, 6:E, -1:No Point)		2	
Diameter (mm)	[dy]	22.054	28.647
Relative radius of curvature (mm)	[pred]	2.434	
Flank pressure (N/mm ²)	[pH]	729.176	
Flank pressure (N/mm ²)	[pdyn]	995.502	
Minimal specific film thickness (µm)	[lamGFY]	0.130	(hY=0.078
µm)			
Safety against micropitting	[Slam(B)]	0.912	

(For intermediate results refer to file: Micropitting_12.tmp)

Pairing Gear 2-3:

Calculation of permissible specific film thickness

Material coefficient	[WW]	0.75
Permissible specific film thickness (µm)	[lamGFP]	0.107

Interim results in accordance with ISO/TR 15144:2014

Coefficient of friction	[mym]	0.078
Lubricant factor	[XL]	1.000
Roughness factor	[XR]	1.254
Tooth mass temperature (°C)	[theM]	70.7
Tip relief factor	[XCa (A)]	1.779
Loss factor	[HV]	0.052
Equivalent Young's modulus (N/mm ²)	[Er]	226374
Compressed viscosity index (m ² /N)	[alf38]	0.02162
Dynamic viscosity (Ns/m ²)	[etatM]	42.8
Roughness average value (µm)	[Ra]	0.8

Calculation of speeds, load distribution and flank curvature according to method B following ISO/TR 15144-1:2014

Ca taken as optimal in the calculation (0=no, 1=yes)		0	0
Calculation at point (0:A, 1:AB, 2:B, 3:C, 4:D, 5:DE, 6:E, -1:No Point)			0
Diameter (mm)	[dy]	26.076	-76.489
Relative radius of curvature (mm)	[pred]		2.422
Flank pressure (N/mm ²)	[pH]		422.084
Flank pressure (N/mm ²)	[pdyn]		634.551
Minimal specific film thickness (μm)	[lamGFY]		0.088 (hY=0.072)
μm)			
Safety against micropitting	[Slam(B)]		0.816
(For intermediate results refer to file: Micropitting_23.tmp)			

The calculation of micropitting specified in ISO15144 is not designed for use with internal toothing because it has not yet been subject to sufficient investigation.
The results can only be used for information purposes.

4c. Safety of the hardened layer (EHT) according to DNV41.2:2012

Required hardening depth EHT (mm)	[t550]	0.10/ 0.11	0.10/ 0.11
0.00/	0.00		
Required hardness at t550 (HV)	[HV.t]	550	550
550			
Condition for hardness on the surface (HV)	[HV.0]	> 463 (HRC46)	> 294 (HRC29)
>	0 (HRC	0)	
HV.0 calculated with SH = min(1.2, SEHT), tz/aH = 0.5			
Safety of the hardened layer	[SEHT]	1.71	1.71/ 2.00
0.00			
Required safety	[SHssmin]	0.90	0.90
0.90			
Result		3	3
-1			
(-1:Not checked 0:EHT too small 1:EHT too large or HV.0 too low		2:EHT too large (> 0.25*mn)	
3:Proof performed and fulfilled, 4:Proof performed but not fulfilled)			

4d. Tooth flank fracture according to ISO DTR 19042-1

Calculation according to Method B			
Calculation at point (0:A, 1:AB, 2:B, 3:C, 4:D, 5:DE, 6:E, -1:No Point)		4	4/ 4
-1			
Diameter (mm)	[dy]	23.64	27.09/ 28.03
0.00			
Relative radius of curvature (mm)	[pred]	2.60	2.60/ 4.29
0.00			
Flank pressure (N/mm ²)	[pH]	705.64	705.64/ 549.02
0.00			
Flank pressure (N/mm ²)	[pdyn]	963.36	963.36/ 825.39

0.00			
Required hardening depth EHT (mm)	[t550]	0.10/ 0.11	0.10/ 0.11
0.00/	0.00		
The calculation is performed with the minimum hardening depth			
Core hardness (HV)	[HV _{core}]	342	342
252			
Hardness curve from: ISO/DTR 19042, chapter 7.3.2			
Maximum utilization	[AFF _{max}]	0.40	0.40/ 0.49
0.00			
Depth of maximum load (mm)	[y]	-0.23	-0.23/ -0.21
0.00			
Material shear strength (N/mm ²)	[τ _{per}]	160.04	160.04/ 164.10
0.00			
Equivalent shear stress (N/mm ²)	[τ _{eff}]	58.33	58.33/ 74.12
0.00			
Safety	[SFF]	1.85	1.85/ 1.65
0.00			
1 = thresholds for applying the method exceeded		1	1
0			
(500 ≤ pH ≤ 3000 N/mm ² ; 5 ≤ pred ≤ 150 mm; 0.3 ≤ t550 ≤ 4.5 mm)			

6. MEASUREMENTS FOR TOOTH THICKNESS

		----- Gear 1 -----	Gear 2 -----	Gear
3 ---				
Tooth thickness deviation	DIN 3967 cd25	DIN 3967 cd25	DIN 3967 cd25	
Tooth thickness allowance (normal section) (mm)	[As.e/i]	-0.054/ -0.084	-0.054/ -0.084	
-0.070/	-0.110			
Number of teeth spanned	[k]	4.000	4.000	
-10.000				
(Internal toothing: k = (Measurement gap number)				
Base tangent length (no backlash) (mm)	[Wk]	10.954	11.006	
-29.633				
Actual base tangent length ('span') (mm)	[Wk.e/i]	10.903/ 10.875	10.955/ 10.927	
-29.699/	-29.736			
Diameter of contact point (mm)	[dMWk.m]	23.365	27.630	
-78.221				
Theoretical diameter of ball/pin (mm)	[DM]	1.938	1.872	
1.682				
Eff. Diameter of ball/pin (mm)	[DM _{eff}]	2.000	2.000	
1.750				
Theor. dim. centre to ball (mm)	[MrK]	12.969	15.479	
-37.959				
Actual dimension centre to ball (mm)	[MrK.e/i]	12.919/ 12.890	15.426/ 15.396	

-38.048/ Diameter of contact point (mm) -78.562	-38.099 [dMMr.m]	22.883	27.929
Diametral measurement over two balls without clearance (mm) -75.901	[MdK]	25.939	30.909
Actual dimension over balls (mm) -76.080/	[MdK.e/i] -76.182	25.837/ 25.781	30.803/ 30.744
Actual dimension over rolls (mm) -76.080/	[MdR.e/i] -76.182	25.837/ 25.781	30.803/ 30.744
Actual dimensions over 3 rolls (mm) -76.064/	[Md3R.e/i] -76.166	0.000/ 0.000	30.754/ 30.695
Tooth thickness (chordal) in pitch diameter (mm) 1.029	[sn]	1.901	1.883
(mm) 0.959/ 0.919	[sn.e/i]	1.847/ 1.817	1.829/ 1.799
Reference chordal height from da.m (mm) 0.249	[ha]	1.407	1.373
Tooth thickness (Arc) (mm) 1.029	[sn]	1.904	1.885
(mm) 0.959/ 0.919	[sn.e/i]	1.850/ 1.820	1.831/ 1.801
Backlash free center distance (mm) -25.539	[aControl.e/i]	25.176/ 25.106	-25.454/
Backlash free center distance, allowances (mm) -0.239	[jta]	-0.124/ -0.194	-0.154/
dNf.i with aControl (mm) -80.571	[dNf0.i]	21.183	25.816
Reserve (dNf0.i-dFf.e)/2 (mm) 0.041	[cF0.i]	0.071	-0.070
Tip clearance 0.099	[c0.i(aControl)]	0.130	0.130
Centre distance allowances (mm) .011	[Aa.e/i]	0.011/ -0.011	0.011/ -0
Circumferential backlash from Aa (mm) .008	[jtw_Aa.e/i]	0.010/ -0.010	0.008/ -0
Radial clearance (mm) .144	[jrw]	0.205/ 0.113	0.249/ 0
Circumferential backlash (transverse section) (mm) .117	[jtw]	0.183/ 0.102	0.205/ 0
Normal backlash (mm) .110	[jnw]	0.172/ 0.096	0.192/ 0

Total rotation angle (°) [j.tSys] 0.4190/ 0.2685
(j.tSys: Rotation angle of planet carrier when driving shaft is fixed)

7. GEAR ACCURACY

	----- Gear 1 -----	Gear 2 -----	Gear 3 ---
According to ISO 1328:1995			
Accuracy grade	[Q-ISO1328]	6	6
6			
Single pitch deviation (µm)	[fptT]	7.00	7.00
7.50			
Base circle pitch deviation (µm)	[fpbT]	6.60	6.60
7.00			
Sector pitch deviation over k/8 pitches (µm)	[Fpk/8T]	9.50	10.00
14.00			
Profile form deviation (µm)	[ffaT]	5.50	5.50
6.50			
Profile slope deviation (µm)	[fHaT]	4.60	4.60
5.50			
Total profile deviation (µm)	[FaT]	7.50	7.50
8.50			
Helix form deviation (µm)	[ffbT]	6.50	6.50
6.50			
Helix slope deviation (µm)	[fHbT]	6.50	6.50
6.50			
Total helix deviation (µm)	[FbT]	9.00	9.00
9.50			
Total cumulative pitch deviation (µm)	[FpT]	20.00	20.00
26.00			
Runout (µm)	[FrT]	16.00	16.00
21.00			
Single flank composite, total (µm)	[FisT]	36.00	35.00
43.00			
Single flank composite, tooth-to-tooth (µm)	[fisT]	16.00	14.00
17.00			
Radial composite, total (µm)	[FidT]	21.00	21.00
26.00			
Radial composite, tooth-to-tooth (µm)	[fidT]	5.00	5.00
5.00			
Axis alignment tolerances (recommendation acc. ISO TR 10064:1992, Quality 6)			
Maximum value for deviation error of axis (µm)	[fSigbet]		5.85
5.85			
Maximum value for inclination error of axes (µm)	[fSigdel]		11.70
11.70			

8. ADDITIONAL DATA

Weight - calculated with da (g) 16.99	[Mass] 58.44	13.47	
Total weight (g) .87	[Mass]		122
Moment of inertia (System referenced to wheel 1): calculation without consideration of the exact tooth shape			
single gears ((da+df)/2...di) (kg*m ²) .759e-006 8.314e-005	[TraeghMom]	8.652e-007	1
System ((da+df)/2...di) (kg*m ²)	[TraeghMom]	4.857e-006	
Mean coeff. of friction (acc. Niemann) .117	[mum]	0.139	0
Wear sliding coef. by Niemann .413	[zetw]	0.755	0
Meshpower (W) .444		544.444	544
Gear power loss (W) .111		3.682	1
Total power loss (W)		14.378	
Total efficiency		0.979	

9. DETERMINATION OF TOOTH FORM

Data for the tooth form calculation :
Data not available.

10. SERVICE LIFE, DAMAGE

Required safety for tooth root	[SFmin]	1.20
Required safety for tooth flank	[SHmin]	0.90

Service life (calculated with required safeties):

System service life (h) [Hatt] > 1000000

Tooth root service life (h) [HFatt] 1e+006 1e+006
1e+006

Tooth flank service life (h) [HHatt] 1e+006 1e+006
1e+006

Note: The entry 1e+006 h means that the Service life > 1,000,000 h.

Damage calculated on basis of required service life (20000.0 h)

F1%	F2%	F3%	H1%	H2%	H3%
0.00	0.00	0.00	0.00	0.00	0.00

REMARKS:

- Specifications with [e/i] imply: Maximum [e] and Minimal value [i] with consideration of all tolerances
 Specifications with [m] imply: Mean value within tolerance
- For the backlash tolerance, the center distance tolerances and the tooth thickness deviation are taken into account. Shown is the maximal and the minimal backlash corresponding the largest resp. the smallest allowances
 The calculation is done for the Operating pitch circle..
- Details of calculation method:
 cg according to method B
 KV according to method B
 KHb, KFb according method C
 fma following equation (64), Fbx following (52/53/56)
 fsh calculated by exactly following the method in Annex D,
 ISO 6336-1:2006
 Literature: Journal "Antriebstechnik", 6/2007, p.64.
 KHa, KFa according to method B
- For the coefficients ZL, ZV, ZR, ZW, ZX, YdreIT, YRreIT and YX, the logarithmically interpolated value taken from the values for the fatigue strength and the static strength based on the number of load cycles is used..

End of Report
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